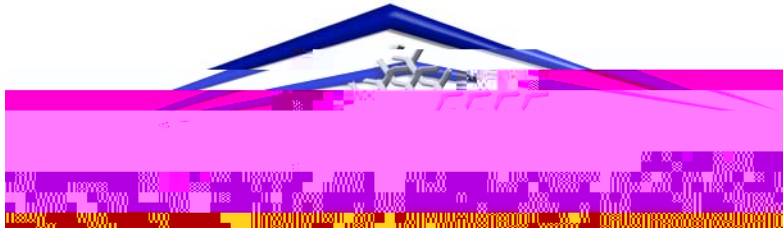


FYdcfh'Bc.'75A!FD!&\$%-!\$()'FYj'B#7''
FYdcfh'8UhY.'8YWY a VYf' %-ž&\$%-

-
-
-
-



Gc`jUm'fl : cf a Yf`m'7mhYWL`) '&\$!%'H*)\$' '_!DK`
ZUVf]W'k]h\`' * i `F7`
9e i]jU`YbWm` AUhYf]U`DfcdYfhm`8UhU`FYdcfh`
Zcf`@U a]bUhY`FYdU]f`DfYdfY [`6UhW\`

B75AD`Dfc^YWh`Bi a VYf.`BDB`\$'%, \$%'

B75AD`HYgh`FYdcfh`Bi a VYf.`75A!FD!&\$%-!\$()'FYj'B#7

FYdcfh'8UhY.'8YWY a VYf' %-ž&\$%-`

HYgh]b [` : UW]]hm.`
National Institute for Aviation Research
Wichita State University
1845 N. Fairmount
Wichita, KS 67260-0093

HYgh`DUbY` : UVf]WUh]cb` : UW]]hm.`
National Institute for Aviation Research - NCAT
Wichita State University
4004 North Webb Road
Wichita, KS 67226

8]ghf]V i h]cb`GhUhY a Ybh`5" Approved for public release; distribution is unlimited.

5HSRUW 1R &\$0 53
5HSRUW 'DWH 'HFHPEHU

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%%` GWcdY`

The test methods and results described in this document are intended to provide basic composite properties essential to most methods of analysis and are consistent with CMH-17-1G—Composite Materials Handbook for Polymer Matrix Composites. This report contains material property data of common usefulness to wide range of projects. The lamina and laminate material property data have been generated with NCAMP oversight in accordance with NSP 100 NCAMP Standard Operating Procedures; the test panels and test specimens have been inspected by NCAMP Authorized Inspection Representatives (AIR) and the testing has been witnessed by NCAMP Authorized Engineering Representatives (AER). However, the data may not fulfill all the needs of any specific company's program; specific properties, environments, laminate architecture, and loading situations may require additional testing.

The use of NCAMP material and process specifications does not guarantee material or structural performance. Material users should be actively involved in evaluating material performance and quality including, but not limited to, performing regular purchaser quality control tests, performing periodic equivalency/additional testing, participating in material change management activities, conducting statistical process control, and conducting regular supplier audits.

The applicability of NCAMP material property data, material allowables, and specifications must be evaluated on a case-by-case basis by aircraft companies and certifying agencies. NCAMP assumes no liability whatsoever, expressed or implied, related to the use of the material property data, material allowables and specifications.

This report contains material property data only. Equivalency statistical analysis data is given in NCP-RP-2018-017 Rev N/C and engineering basis values generated from material qualification testing can be obtained from NCP-RP-2012-023 Rev N/C or later revisions. The equivalency material was procured to NCAMP Material Specification NMS 532/6 Rev A Release dated September 19, 2016. The equivalency test panels were cured in accordance with NCAMP Process Specification NPS 85321 Revision C dated May 31, 2018 Baseline “C” Cure Cycle. The NCAMP Test Plan NTP 5325QR1 was used for this equivalency program.

Part fabricators that wish to utilize the material property data, allowables and specifications may be able to do so by demonstrating the capability to reproduce the original material properties; a process known as equivalency. More information about this equivalency process including the test statistics and its limitations can be found in Section 6 of DOT/FAA/AR-03/19 and Section 8.4.1 of CMH-17-1G. The applicability of equivalency process must be evaluated on program-by-program basis by the applicant and certifying agency. The applicant and certifying agency must agree that the equivalency test plan, along with the equivalency process described in Section 6 of DOT/FAA/AR-03/19 and Section 8.4.1 of CMH-17-1G, are adequate for the given program.

Aircraft companies should not use the data published in this report without specifying NCAMP Material Specification NMS 532/6. NMS 532/6 have additional requirements that are listed in its prepreg process control document (PCD), fiber specification, fiber PCD and other raw material specifications and PCDs which impose essential quality controls on the raw materials and raw material manufacturing equipment and processes. Aircraft companies and certifying agencies should assume that the material property data published in this report is not applicable when the material is not procured to NMS 532/6. NMS 532/6 is a free, publicly available, non-proprietary aerospace industry material specification.

The data in this report is intended for general distribution to the public, either freely or at a price that does not exceed the cost of reproduction (e.g. printing) and distribution (e.g. postage).

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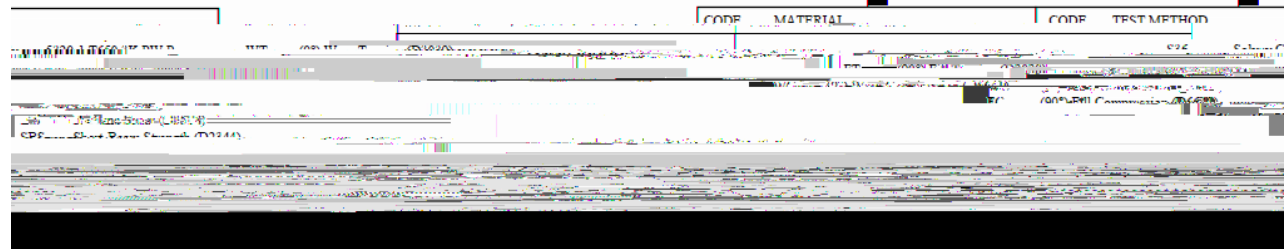
- Q₂^t major Poisson's ratio, tension
- P H micro-strain
- E₁^c compressive modulus, longitu

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.....75 A!FDI&\$%-!\$()'FYj'B#7

%"'' B=5 FËGdYW] a Yb'BU a]b [' : cf a Uh'

NAMING FORMAT



:] [i fY'%!%. 'AUhYf]U'BU a]b [' : cf a Uh'

8YWy a VYf %-ž&\$%-75A!FD!&\$%-!\$()'FYj'B#7

%"(' FYZYfYbWYg'

5GHA'GhUbXUfXg'

All testing was in accordance

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%")` AYh\cXc`c [m`

%")" %` DfcWYgg`8YZ]b]h]cb`

A single batch of prepreg was used to demonstrate equivalency. These single batch tests are designed to demonstrate equivalency with the original three batches qualification data for purposes described in CMH-17-1G Section 8.4.1 and DOT/FAA/AR-03/19 Section 6.

For each combination of test, batch and condition, the specimens were selected from a minimum of two separate panels cured separately as shown in Figure 1-2 unless

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:][i fY`%!`.GdYW]a Yb`HfUWYUV]`]hm`@]bY`

8YWY a VYf %-ž&\$%-75 A!FD!&\$%-!\$()`FYj`B#7

%)"&`GdYW] a Yb` /`HYgh]b [`8YhU]`g`

%)"&%"`HUVV]b [`

Tabs were not used for this program.

%)"&`&`

%") "'HYgh' AUhf]I'

The table below shows lay-ups and test matrices used for lamina and laminate level testing on the single batch equivalency of the Solvay 5320-1 T650 3k PW prepreg material.

| Layup | Test Type and Direction | Property | Number of Batches x Number of Panels x Number of Specimens | | |
|--|---|---|--|-----------------|--------------|
| | | | Test Temperature/ Moisture Condition | | |
| | | | CTD | RTD | ETW2 |
| [0] ₁₅ | ASTM D3039 Warp Tension | Strength, Modulus and Poisson's Ratio | 1x2x4 | 1x2x4 (4) | 1x2x4 |
| [0] ₁₅ | ASTM D6641 Warp Compression | Strength, Modulus and Poisson's Ratio | 1x2x4 | 1x2x4 (1)(4) | 1x2x4 (3) |
| [90] ₁₅ | ASTM D3039 Fill Tension | Strength and Modulus | 1x2x4 | 1x2x4 (4) | 1x2x4 |
| [90] ₁₅ | ASTM D6641 Fill Compression | Strength and Modulus | 1x2x4 | 1x2x4 (1)(4) | 1x2x4 (3) |
| [45/-45] _{3S} | ASTM D3518 In-Plane Shear (2) | Strength and Modulus | 1x2x4 | 1x2x4 (4) | 1x2x4 |
| [0] ₃₂ | ASTM D2344 Short Beam | Strength | 1x2x4 | 1x2x4 | 1x2x4 |
| (25/50/25 - QI) [45/0/-45/90]2S | ASTM D5766 Open-Hole Tension | Strength | | 1x2x4 | 1x2x4 |
| (25/50/25 - QI) [45/0/-45/90/45/0/- 45/90/-45/90]S | ASTM D6484 Open-Hole Compression (5) | Strength | | 1x2x4 (1) | 1x2x4 |
| (25/50/25 - QI) [45/0/-45/90]3S | ASTM D7136 & D7137 Compression After Impact (1500 in/lb/in) | Strength | | 1x2x4 | |

HUV'Y'!%. '9e i]jU'YbWm'HYgh' AUhf]I'

BchY'. Back-to-back strain gages are needed on the first two specimens. If no buckling is observed, the remaining modulus specimens will require a strain gage on one side of the specimens only. An appropriate extensometer may be used in place of the strain gage.

BchY'&. Gripped (tab) length is 1.5±0.5" on each end of the 10" long specimen. Once the samples have reached the 5% strain level, the actuator/crosshead displacement rate can be increased by four times the initial rate. Continue testing at the higher strain rate until ultimate failure is observed.

BchY' . If strain gage is used for modulus measurement, a separate un-gaged specimen must be used for strength measurement; because the strain gage and its protective coating may prevent moisture absorption in the gage area.

BchY' (. At least two specimens must be gaged to obtain full stress-strain curve to failure. An appropriate extensometer may be used in place of the strain gage for the remaining specimens.

BchY'). Open-hole configuration: 0.25" hole diameter, 1.5" width.

8YWy a VYf %-ž&\$%- *****75A!FD!&\$%-!\$()'FYj'B#7

Table 1-1 shows the single batch of the Solvay 5320-1 T650 3k PW prepreg test matrix. The layup angles 0°, 45°, -45° and 90° refer to the orientation of the warp direction. The laminate stacking sequences in this program are not specific to any design. Therefore, careful consideration should be given to the validity of properties derived from this program based on the design specific laminates in a structure to be certified.

%)" (' 7 ifYX'@Ua]bUhY'D\mg]WU''HYgh]b ['

The properties in Table 1-2 were determined for each panel used for test coupons with the exception of Tg by DMA which were conducted on one laminate per batch from each oven cure conducted where that batch is present. The tests were performed by the National Institute for Aviation Research (NIAR) Composites Laboratory under the supervision of NCAMP.

DfcdYfhm'

7cbX]h]cb#AYh\cX'

%")"*' Bcb!U a V]Ybh'HYgh]b ['

The chamber was of adequate size so that all test fixtures and load frame grips were contained within the chamber.

For elevated temperature testing, the temperature chamber, test fixture, and grips were preheated to the specified temperature. Each specimen was heated to the required test temperature as verified by a thermocouple in direct contact with and taped to the specimen gage section. The heat-up time of the specimen did not exceed 5 minutes, unless otherwise specified in individual test summary sheets. The test was started 5 ¹/₀ minutes after the specimen reached the test temperature. During the test, the temperature, as measured on the specimen, was within $\pm 5^\circ\text{F}$ of the required test temperature.

For subzero temperature testing, each specimen was cooled to the required test temperature as verified by a thermocouple in direct contact with and taped to the specimen gage section. The test started 5 ¹/₀ minutes after the specimen reached the test temperature. During the test, the temperature, as measured on the specimen, was within $\pm 5^\circ\text{F}$ of the required test temperature.

For wet specimens, the moisture loss was determined by subjecting representative specimens to the same amount of time required to heat-up and fail the specimens. For filled-hole or bearing specimens, fasteners were removed prior

%)"+'Bcf a U`nUh]cb'DfcWYX i fYg'

Most lamina level tension and compression strength and modulus properties, and all laminate level properties were normalized according to nominal cured ply thickness. Lamina level properties that were not normalized include 90° tensile strength and modulus (unidirectional only), 90° compressive strength and modulus (unidirectional only), in-plane shear strength and modulus, Poisson's ratio, SBS, and ILT. After normalizing, data scatter reduced or remained the same. If data scatter increased significantly after normalizing, the reason was investigated. Wherever properties are normalized, both measured and normalized data were reported.

The average cured ply thickness of 0.0077 inches has been used as the nominal cured ply thickness (CPT) for normalization purpose. This value was used in the normalization of data in the qualification program. The following normalization formula was used:

$$\text{Normalized Value} = \text{Measured Value} \times \text{Measured CPT} / \text{Nominal CPT}.$$

%)", '=bgdYWh]cb' JYf]Z]WUh]cb'

The 1-batch equivalency panels have been fabricated according to the requirements of the test plan and conformed by an NCAMP AIR. The test specimens and test setup have also been conformed by an NCAMP AIR.

Testing was witnessed by NCAMP. Test setup and witnessing was delegated to an NCAMP AER. Mechanical testing was carried out at the National Institute for Aviation Research, Wichita State University.

%)"- 'AUhYf]U`DYX] [fYY'=bZcf a Uh]cb'

The PMC Data Collection Template includes the material pedigree information required, such as material and batch information, as well as panel fabrication record, environmental conditioning, test equipment, and test procedures.

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&"` HYgh`FYg i`hg`

&"%` @Ua JbU`@YjY`HYgh`G i a a Ufm`

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$()`FYj`B#7

&"'' =bX]j]X i U`HYgh'G i a a Uf]Yg`

&" "%' KUfd'HYbg]cb'DfcdYfh]Yg'fl KHL`

| | | | | | | | | |
|---|---------------------------------|--|--|--|--|--|--|--|
| A U h Y f] U` Solvay 5320-1 T650 3k-PW fabric with 36% RC | | | | | | HYbg]cbž' %!U]jg` Solvay 5320-1 T650 3k-PW fabric with 36% RC [0]15 | | |
| FYg]b`Wcb]Ybh. :]VYf`jc`i`a`Y. D`m`Wc`i`bh. | 37.53 %wt 54.83 %vol 15 | 7 c a d`X`Ybg]lm. 1.553 g/cc | | | | | | |
| HYgh`a`Yh`c`X. Bc`f`a`U`]n`Y`X`V`m. | ASTM D3039-17 0.0077 in. CPT | Ac`X`i`i`g`WU`Wi`U`h]cb. 1000-3000 microstrain | | | | | | |
| | | 7H8 | | FH8 | | 9HK& | | |
| HYgh`HY`a`d`Yf`U`h`i`f`Y`š`: Ac]gh`i`f`Y`7`cbX]h]cb]b[9e`i`]Vf]i`a`U`h`H`F`< Gc`i`f`WY`Wc`X`Y`d`f`Y`Z]i`Y`X`V`m`NTP-5325QRI-SOL-S36-NIAR- | | -65 Dry WT-X-CX-1-CTD-X | | 70 Dry WT-X-CX-1-RTD-X | | 250 Equilibrium 160 F,85% WT-X-CX-1-ETW2-X | | |
| | | Bc`f`a`U`]n`Y`X` | AYug`i`f`Y`X` | Bc`f`a`U`]n`Y`X` | AYug`i`f`Y`X` | Bc`f`a`U`]n`Y`X` | AYug`i`f`Y`X` | |
| AYub A]b]a`i`a` AUI]a`i`a` 7`J`fl`i`l` | | 108.021 105.173 111.779 2.222 | 109.315 106.713 113.515 2.238 | 121.316 118.808 124.669 1.662 | 122.606 119.498 126.754 1.929 | 135.410 129.038 140.538 2.473 | 136.203 130.257 142.805 2.774 | |
| Bc`Gd`YW]a`Ybg Bc`Df`Yd`f`Y`[`@`c]g` | | 8 1 | | 9 1 | | 16 1 | | |
| AYub A]b]a`i`a` AUI]a`i`a` 7`J`fl`i`l` | | 9.806 9.728 9.908 0.637 | 9.923 9.838 10.062 0.717 | 9.755 9.663 9.902 0.688 | 9.858 9.775 10.068 0.948 | 9.751 9.487 9.971 1.483 | 9.809 9.456 10.140 2.253 | |
| Bc`Gd`YW]a`Ybg Bc`Df`Yd`f`Y`[`@`c]g` | | 8 1 | | 9 1 | | 16 1 | | |
| AYub A]b]a`i`a` AUI]a`i`a` 7`J`fl`i`l` | | | 0.054 0.049 0.060 7.419 | | 0.049 0.042 0.055 7.228 | | 0.046 0.034 0.051 11.600 | |
| Bc`Gd`YW]a`Ybg Bc`Df`Yd`f`Y`[`@`c]g` | | 8 1 | | 9 1 | | 8 1 | | |

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$()`FYj`B#7

8YWy a VYf %-ž&\$%-75A!FD!&\$%-!\$()'FYj'B#7

&"'''' KUfd'7c a dfYgg]cb'DfcdYfh]Yg'fl K 7Ł'

AUyYfJU'.

FYgjb'WcbhYbh. 37.60 %wt



&"")'=b!D`UbY`G\YUf`DfcdYfh]Yg`fl=DGL`

AUhYfjU`.

FYgjb`WcbhYbh. 37.09 %wt
:jVYf`jc`i aY. 55.12 %vol
D`m`Wc i bh. 12

7c a d`XYbg]hm. 1.551 g/cc

HYgh`a Yh\cX. ASTM D3518-18

AcXi`i`g`WU`Wi`U]jcb.` 2000-6000 microstrain

BcfaU`]nYX`Vm. NA

| | BcfaU`]nYX | AYUg ifYX | BcfaU`]nYX | AYUg ifYX | BcfaU`]nYX | AYUg ifYX |
|------------------------|------------|-----------|------------|-----------|------------|-----------|
| AYUb | | 11.536 | | 8.322 | | 3.523 |
| A]b]a i a | | 11.169 | | 8.230 | | 3.434 |
| AU]a i a | | 11.788 | | 8.415 | | 3.633 |
| 7`J`fi i Ł | | 1.703 | | 0.630 | | 1.870 |
| Bc`GdY]a Ybg | | | | | | |
| Bc`DfYdfY[`@chg | | | | | | |
| AYUb | | 18.308 | | 14.455 | | 6.712 |
| A]b]a i a | | 17.843 | | 14.289 | | 6.549 |
| AU]a i a | | 18.761 | | 14.700 | | 6.968 |
| 7`J`fi i Ł | | 2.137 | | 0.835 | | 2.182 |
| Bc`GdY]a Ybg | | | | | | |
| Bc`DfYdfY[`@chg | | | | | | |
| AYUb | | 0.847 | | 0.726 | | 0.365 |
| A]b]a i a | | | | | | |



8YWy a VYf %-ž&\$%-`

&"'+ Í&)#)\$&) Î`CdYb!<c`Y`HYbg]cb`%`DfcdYfh]Yg`flC<H%L`

| | | | | | |
|--|-------------------------------------|---|-------------------------------------|---|--|
| AUhYfjU` Solvay 5320-1 T650 3k-PW fabric with 36% RC | | | | CdYb!<c`Y`HYbg]cb`% Solvay 5320-1 T650 3k-PW fabric with 36% RC [45/0-/45/90]2S | |
| FYgjb`WcbhYbh. :jVYf`jc`i aY. D`m`Wc i bh. | 37.65 % wt 54.40 % vol 16 | 7ca d`XYbg]hm. 1.544 g/cc | | | |
| HYgh`a Yh\cX. BcfaU`nYX`Vm. | ASTM D5766-11 0.0077 in. CPT | FH8 | | 9HK& | |
| HYgh`HY adYfUhi fY`0s :0 AcjghifY`7cbX]cb]b[9ei]Vf]i a`Uh`H`F< Gc ifWY`WcXY`dfYz]lYX`Vm. NTP-5325QRI-SOL-S36-NIAR- | 70 Dry OHT1-X-CX-1-RTD-X | 250 Equilibrium 160 F,85% OHT1-X-CX-1-ETW2-X | | | |
| | BcfaU`nYX` | AYUg ifYX` | BcfaU`nYX` | AYUg ifYX` | |
| AYUb A]b]a i a AU]a i a C<H%`GhfYb [h\`0_g]0 7`J`i i L | 43.951 40.550 46.590 4.420 | 43.910 40.534 46.634 4.457 | 48.089 46.157 49.744 2.929 | 48.046 46.151 49.663 2.874 | |
| Bc`GdY]a Ybg Bc`DfYdfY[`@chg | 8 1 | | 8 1 | | |

&"", 'Í&)#)\$#&)Î`CdYb!<c`Y`7c a dfYgg]cb`%`DfcdYfh]Yg`flC<7%L`

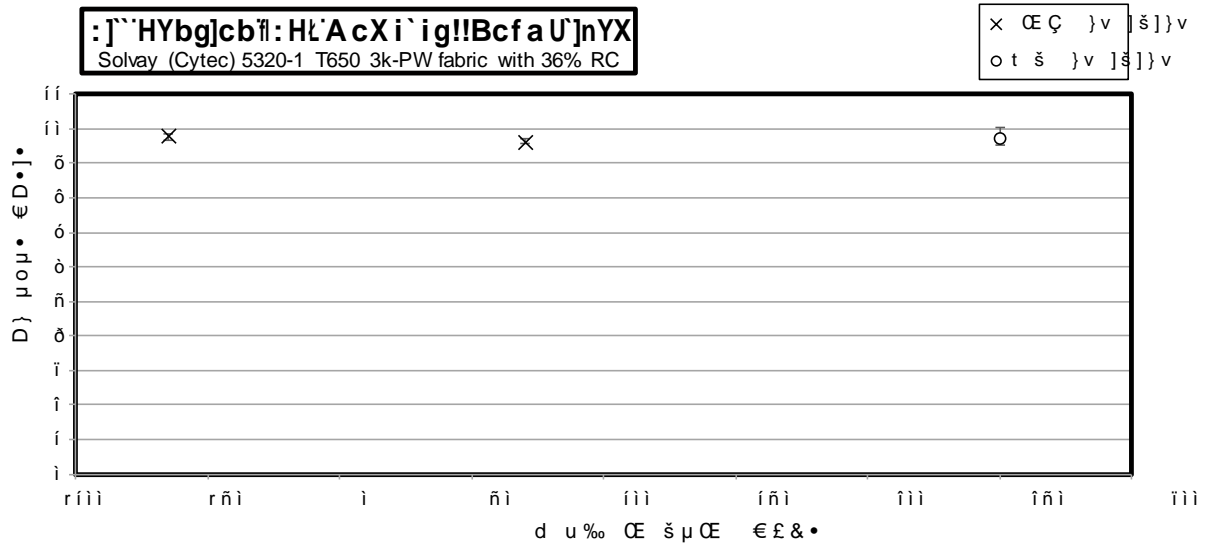
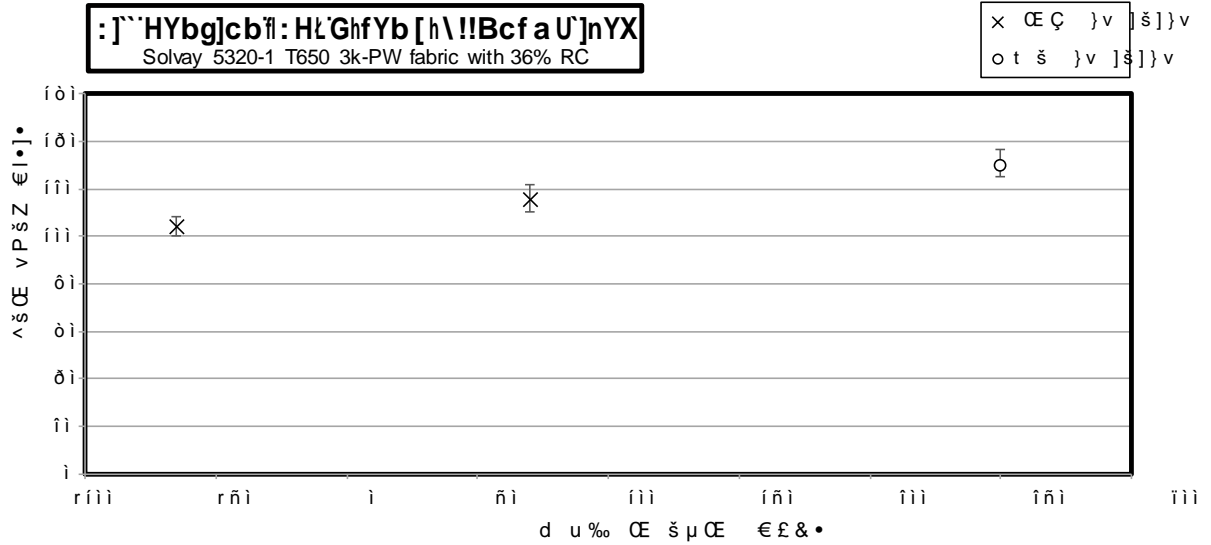
| | | | |
|---|--|--|-------------------------------------|
| AUhYfjU` Solvay 5320-1 T650 3k-PW fabric with 36% RC FYgjb`WcbhYbh. 37.47 %wt :jVYf`jc`i aY. 54.59 %vol D`m`Wc i bh. 20 HYgh`a Yh\cX. ASTM D6484-14 BcfaU`nYX`Vm. 0.0077 in. CPT | | CdYb!<c`Y`7c a dfYgg]cb`%` Solvay 5320-1 T650 3k-PW fabric with 36% RC [45/0/-45/90/45/0/-45/90/-45/90]S | |
| | | FH8 | 9HK& |
| HYgh`HY a dYfUhi fY`S:Q AcjghifY`7cbX]jcb]b[9ei]Vf]i a`Uh`H`F< GcifWY`WcY`dfYz]lYX`Vm. NTP-5325QRI-SOL-S36-NIAR- | | 70 Dry | 250 Equilibrium 160 F,85% |
| | | OHC1-X-CX-1-RTD-X | OHC1-X-CX-1-ETW2-X |
| | | BcfaU`nYX | AYUg ifYX |
| | | BcfaU`nYX | AYUg ifYX |
| AYUb A]b]a i a AU]a i a C<7%GhfYb[h\`0_g] 7`J`i L | | 48.841 47.549 50.365 1.718 | 48.733 47.462 50.099 1.623 |
| | | 34.424 32.504 36.655 3.808 | 34.331 32.316 36.568 3.830 |
| Bc`GdY]a Ybg Bc`DfYdfY[`@chg | | 8 1 | 8 1 |

8YWy a VYf %-ž&\$%-`

8YWy a VYf %-ž&\$%-

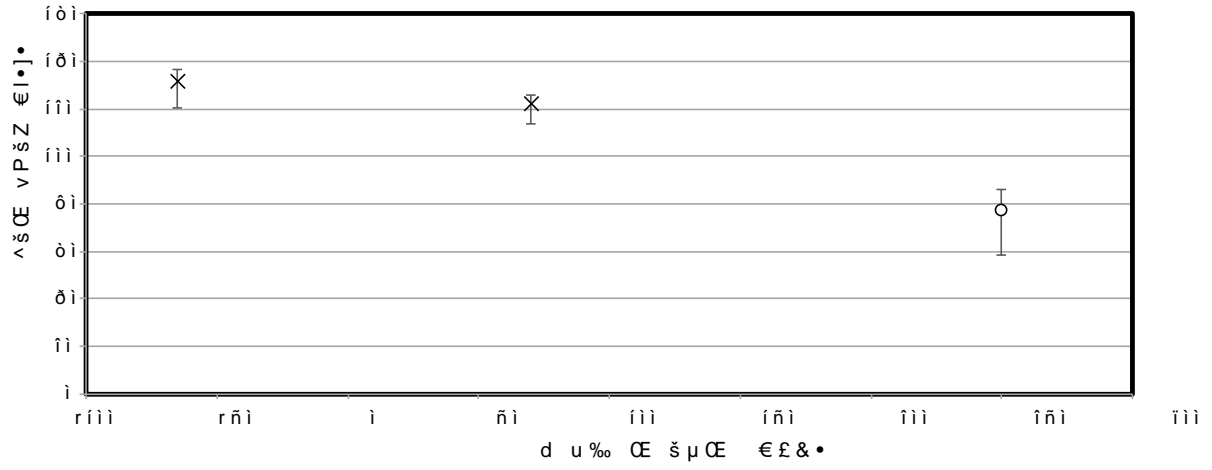
.....75A!FD!&\$%-!\$()`FYj`B#7

'"&' :j''HYbg]cb'DfcdYfh]Yg'fl:Hk'



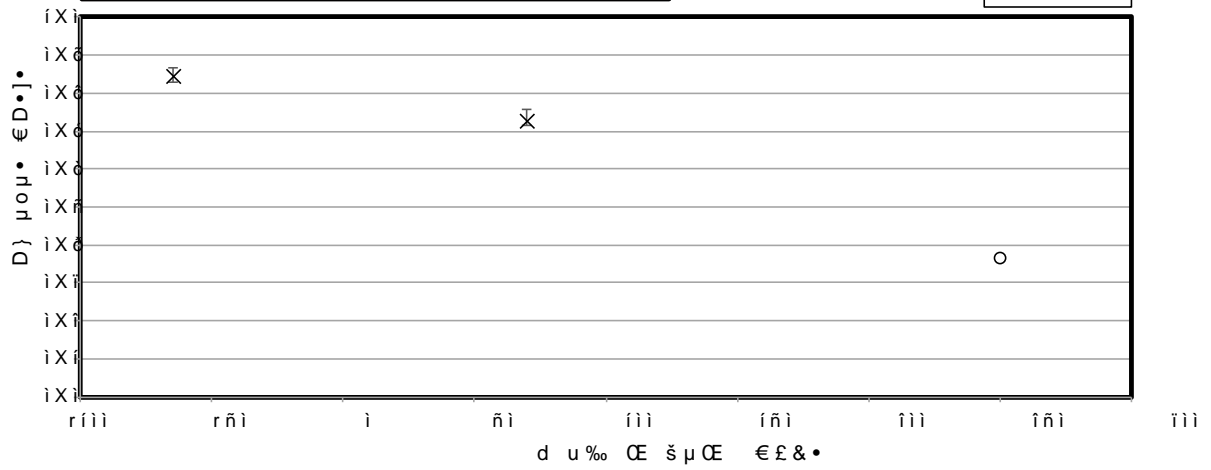
KUfd'7c a dfYgg]cb'DfcdYfh]Yg'flK 7Ł'

KUfd'7c a dfYgg]cb'flK 7Ł'GhfYb [h\!!Bcf aU`nYX
Solvay 5320-1 T650 3k-PW fabric with 36% RC

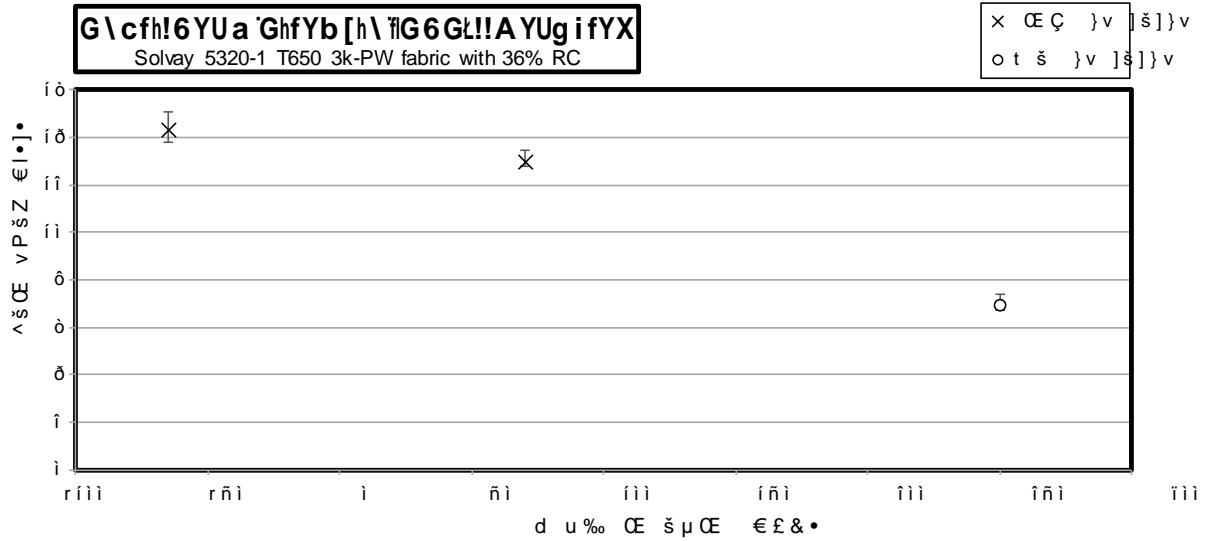


=b!D`UbY'G\YUfñ=DGL'AcXi`ig!!AYUgi fYX
Solvay 5320-1 T650 3k-PW fabric with 36% RC

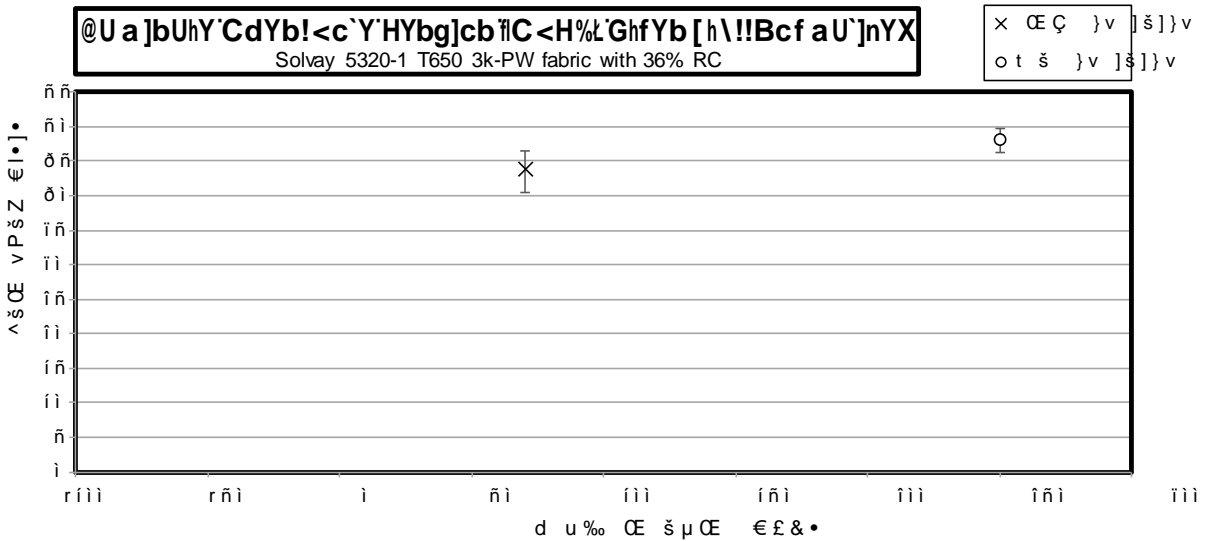
x œ ç }v]š}}v
o t š }v]š}}v



'"*' @U a]bU'G\cfh!6YU a 'GhfYb [h\ 'DfcdYfh]Yg'flG6GŁ'

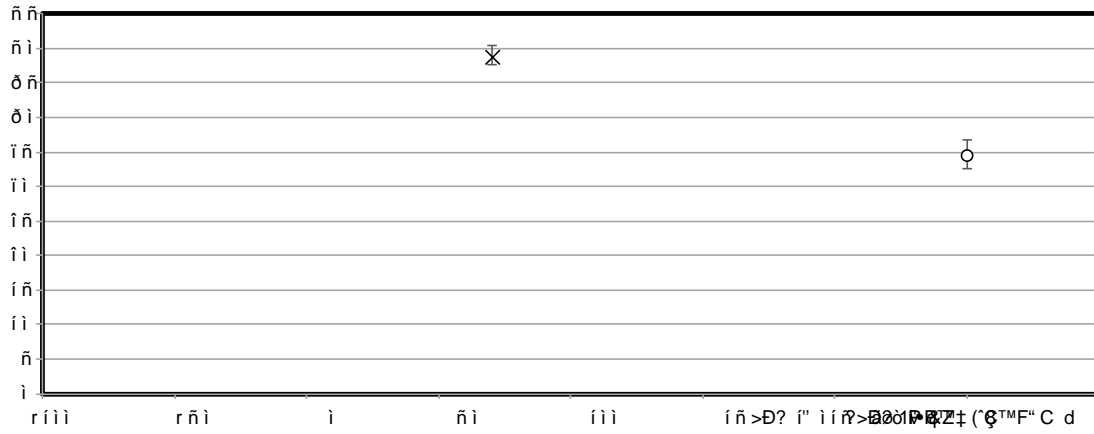


'"+' Í&#) \$#&) Î' CdYb!<c`Y`HYbg]cb`%'DfcdYfh]Yg'flC<H%Ł'



8YWY a VYf %-ž'&\$%- '75 A!FD!&\$%-!\$()'FYj`B#7

'", ' í&)#)\$#&)Î`CdYb!<c`Y`7c a dfYgg]cb`%`DfcdYfh]Yg`flC<7%k`



8YWy aVyf %-ž&\$%- 75A!FD!&\$%-!\$()'FYj'B#7

(" FUK'8UhU'

("%' KUfd'HYbg]cb'DfcdYfh]Yg'flKHL'

bcaU'n]b[
hda

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$()'FYj`B#7

bcf a U'n]b [
h_dm '0]b0
0.0077

GdYw]a Yb`B i a VYf

B-5F`
6Urw\`

B-5F`

8YWy a VYf %-ž&\$%-

.....75 A!FD!&\$%-!\$()'FYj'B#7

bcaU'n]b[
h_{ca}'0]b0
0.0077

| GdYw]a Yb'Bi a VYf | B-5F' 6UhW\` | B-5F' 7 ifY'7mWY | DfYdfY['@ch' | 7 ifY'7mWY' | GfYb[h\ 0_g]0 | AcX1' ig' 0Ag]0 | Dc]ggcblg' FUh]c | 5 j[' GdYw]a Yb' H\]W_bYgg' 0]b0 | 'D]Yg]b' @Ua]bUhY | :U] ifY' AcXY | 5 j['h _{ca} '0]b0 | GfYb[h\ 0_g]0 | AcX1' ig' 0Ag]0 |
|--|-----------------|---------------------|--------------|-------------|------------------|--------------------|---------------------|---|----------------------|------------------|----------------------------|------------------|--------------------|
| NTP-5325QRI-SOL-S36-NIAR-WT-A-C1-1-ETW2-1* | A | C1 | 1 | 1 | 130.488 | 10.083 | | 0.114 | 15 | LGB | 0.0076 | 129.038 | 9.971 |
| NTP-5325QRI-SOL-S36-NIAR-WT-A-C1-1-ETW2-2* | A | C1 | 1 | 1 | 142.794 | 9.946 | | 0.114 | 15 | LGB | 0.0076 | 140.404 | 9.780 |

("& :]'`HYbg]cb'DfcdYfh]Yg'fl : HŁ'

:]'`HYbg]cb'DfcdYfh]Yg'fl : HŁ!!7H8
 GhfYb[h\`/'AcXi`ig
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

bcf a U'n]b[
 hcfm'0]b0
 0.0077

| GdYW]aYb Bi a VYf | B-5F 6UHw\` | B-5F 7i fY'7mWY | DfYdfY['@ch | 7i fY'7mWY | GhfYb[h\ 0_g]0 | AcXi`ig` 0Ag]0 | 5j[`` GdYW]aYb` H\]W_bYgg` 0]b0 | `D]Yg]b` @Ua]bUhY | :U] i fY'AcXY |
|--|----------------|--------------------|-------------|------------|-------------------|-------------------|--|----------------------|---------------|
| NTP5325QR1-SOL-S36-NIAR-FT-A-C1-1R-CTD-1 | A | C1 | 1 | 1 | 103.236 | 9.953 | 0.114 | 15 | LGT |
| NTP5325QR1-SOL-S36-NIAR-FT-A-C1-1R-CTD-2 | A | C1 | 1 | 1 | 105.968 | 9.986 | 0.114 | 15 | LGM |
| NTP5325QR1-SOL-S36-NIAR-FT-A-C1-1R-CTD-3 | A | C1 | 1 | 1 | 106.253 | 9.974 | 0.114 | 15 | LGB |
| NTP5325QR1-SOL-S36-NIAR-FT-A-C1-1R-CTD-4 | A | C1 | 1 | 1 | 106.223 | 9.938 | 0.114 | 15 | LGM |
| NTP5325QR1-SOL-S36-NIAR-FT-A-C2-1R-CTD-1 | A | C2 | 1 | 2 | 101.153 | 9.780 | 0.116 | 15 | LAB |
| NTP5325QR1-SOL-S36-NIAR-FT-A-C2-1R-CTD-2 | A | C2 | 1 | 2 | 107.948 | 9.816 | 0.116 | 15 | LGM |
| NTP5325QR1-SOL-S36-NIAR-FT-A-C2-1R-CTD-3 | A | C2 | 1 | 2 | 107.751 | 9.671 | 0.115 | 15 | LGB |
| NTP5325QR1-SOL-S36-NIAR-FT-A-C2-1R-CTD-4 | A | C2 | 1 | 2 | 99.708 | 9.738 | 0.116 | 15 | LGB |

| 5j[``hcfm'0]b0 | GhfYb[h\ 0_g]0 | AcXi`ig`bca` 0Ag]0 |
|----------------|-------------------|-----------------------|
| 0.0076 | 102.089 | 9.842 |
| 0.0076 | 104.790 | 9.875 |
| 0.0076 | 104.827 | 9.840 |
| 0.0076 | 104.721 | 9.797 |
| 0.0077 | 101.474 | 9.811 |
| 0.0077 | 108.229 | 9.842 |
| 0.0077 | 107.580 | 9.656 |
| 0.0077 | 100.111 | 9.778 |

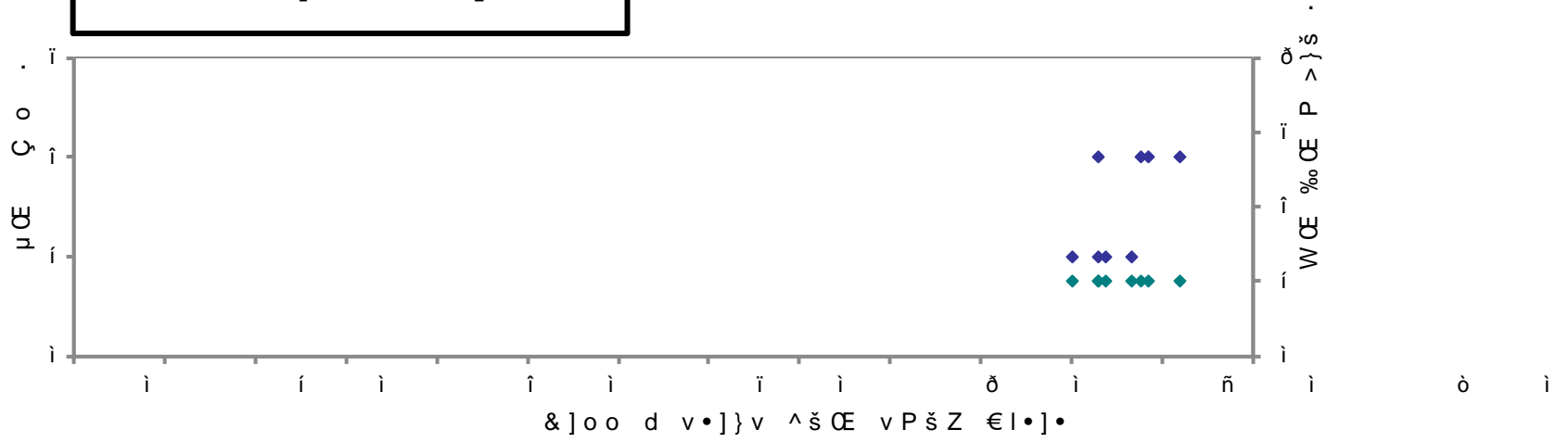
5jYfU[Y %\$(+,\$ -',)+
 GhUbXUfX'8Yj' '\$** \$%&%
 7cYZZ'cZ'JUf'0 i 0 &'&* %&&+
 A]b' --+\$, --*+*
 AUI' %\$+-(, -',+*
 Bi a VYf cZ'GdYW'

5jYfU[Ybcfa \$\$\$++ %\$(&&, -', \$)
 GhUbXUfX'8Yj'bcfa &', \$ \$\$\$*,
 7cYZZ'cZ'JUf'0 i 0bcfa &'&((\$\$\$*-\$
 A]b' \$\$\$+* %\$\$%%% -'*)*
 AUI' \$\$\$++ %\$,'&&- -',+)
 Bi a VYf cZ'GdYW'

8YWy aVYf %-ž&\$%-

.....75A!FD!

:]``HYbg]cb'DfcdYfh]Ygřl: Hł!!FH 8
Bcf a U`]nYX'GhfYb [h\



8YWy a VYf %-ž'&\$%-'

8YWY a VYf %-ž'&\$%-'

.....75 A!FD!&\$%-!\$()'FYj'B#7

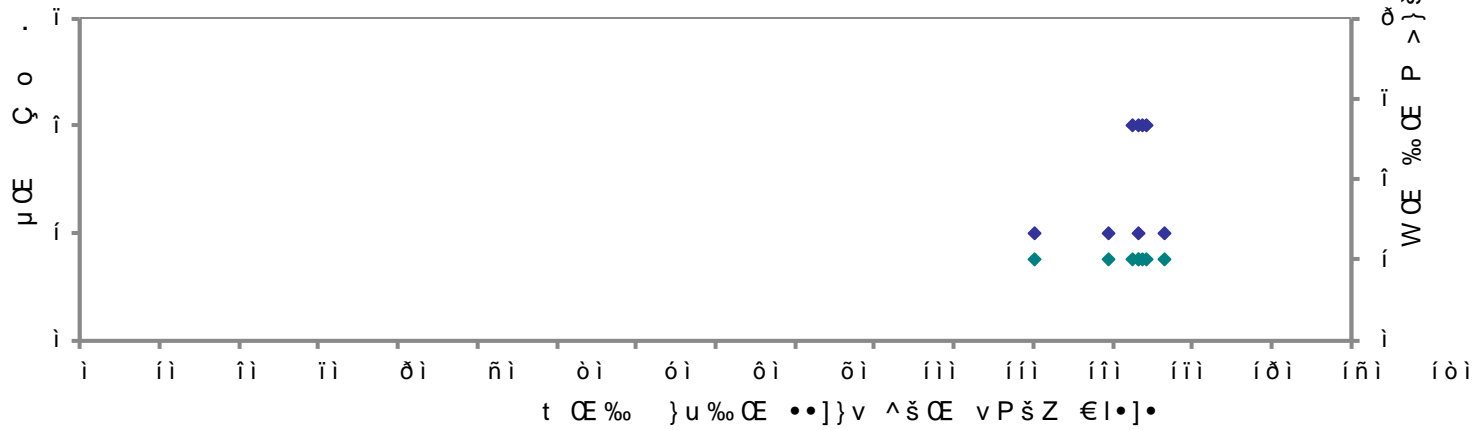
("' K Ufd'7c a dfYgg]cb'DfcdYfh]Yg'flK 7L'

b c f a U'n]b[
h d m'0]b0
0.0077

| GdYW]aYb'Bi a VYf | B-5F' 6UHW\' | B-5F' 7iFY'7mW'Y | DfYdfY['@ch' . | 7iFY'7mW'Y' . | GhfYb[h\ 0_g]0 | AcXi'ig' 0Ag]0 | 5j['' GdYW]aYb' H\]W_bYgg' 0]b0 | 'D]Yg]b' @Ua]bUrY | :U] ifY'AcXY | 5j['''h d m'0]b0 | GhfYb[h\ b c f a' 0_g]0 | AcXi'ig' b c f a' 0Ag]0 |
|--|--------------|------------------|-----------------|---------------|----------------|----------------|---------------------------------|-------------------|--------------|------------------|-------------------------|-------------------------|
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-CTD-1 | A | C1 | 1 | 1 | 122.677 | 9.211 | 0.113 | 15 | BGM | 0.0075 | 120.146 | 9.021 |
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-CTD-2 | A | C1 | 1 | 1 | 138.578 | 9.126 | 0.114 | 15 | BGM | 0.0076 | 136.498 | 8.989 |
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-CTD-3 | A | C1 | 1 | 1 | 135.480 | 8.806 | 0.114 | 15 | BGM | 0.0076 | 133.349 | 8.667 |

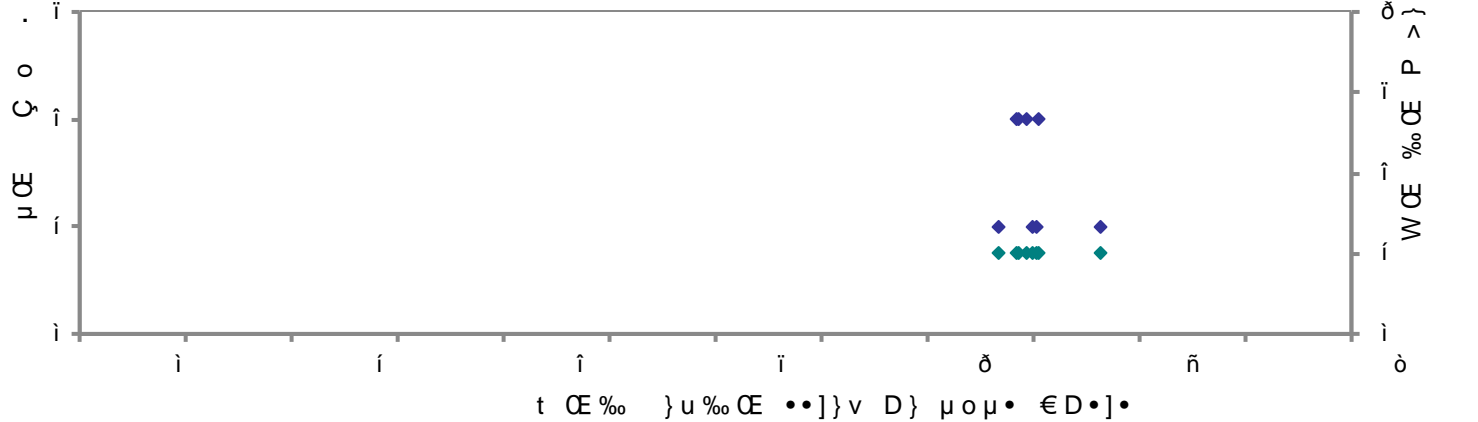
KUfd'7c a dfYgg]cb'DfcdYfh]YgflK7L!!7H8
Bcf a U`nYX'GhfYb[h
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

◆ μ_{CE} ζ_o .
 ◆ $W_{CE} \%_{CE}$ $P > \} \text{š}$.



KUfd'7c a dfYgg]cb'DfcdYfh]YgflK7L!!7H8
Bcf a U`nYX'AcXi`ig
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

◆ μ_{CE} ζ_o .
 ◆ $W_{CE} \%_{CE}$ $P > \} \text{š}$.



8YWy a VYf %-ž&\$%-

.....75 A!FD!&\$%-!\$()'FYj'B#7

KUfd'7c a dfYgg]cb'DfcdYfh]Yg'fK 7L!!FH8
GhfYb[h\ /'AcXi'ig

b c f a U] n] b ['
h d m ' 0] b 0
0.0077

| GdYw]a Yb'Bi a VYf | B:5F' 6UhW\ | B:5F' 7ifY'7mWY | DfYdfY['@ch' 7ifY'7mWY | GhfYb[h\ 0_g]0 | AcXi'ig' 0Ag]0 | 5j[" GdYw]a Yb' H\]W_bYgg' 0]b0 | 'D]Yg]b' @Ua]bUhY | :U] ifY'AcXY | 5j["'h d m ' 0] b 0 | GhfYb[h\ b c f a ' 0_g]0 | AcXi'ig b c f a ' 0Ag]0 | |
|---|-------------|-----------------|------------------------|----------------|----------------|---------------------------------|-------------------|--------------|----------------------|--------------------------|-------------------------|-------|
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-RTD-1* | A | C1 | 1 | 1 | 126.786 | 8.919 | 0.115 | 15 | BGM | 0.0076 | 125.890 | 8.856 |
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-RTD-2* | A | C1 | 1 | 1 | 122.642 | 8.946 | 0.115 | 15 | BGM | 0.0077 | 122.164 | 8.911 |
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-RTD-3 | A | C1 | 1 | 1 | 126.631 | 9.322 | 0.114 | 15 | BGM | 0.0076 | 125.370 | 9.229 |
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C1-1-RTD-4 | A | C1 | 1 | 1 | 123.297 | 9.339 | 0.114 | 15 | BGM | 0.0076 | 121.980 | 9.239 |
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C2-1-RTD-1* | A | C2 | 1 | 2 | 125.575 | 8.942 | 0.115 | 15 | HAT, BAT | 0.0076 | 124.723 | 8.881 |
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C2-1-RTD-2*** | A | C2 | 1 | 2 | | 8.988 | 0.114 | 15 | HIT | 0.0076 | | 8.898 |
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C2-1-RTD-3 | A | C2 | 1 | 2 | 114.577 | 9.007 | 0.115 | 15 | BGM, HAT | 0.0076 | 113.701 | 8.938 |
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C2-1-RTD-4 | A | C2 | 1 | 2 | 121.965 | 8.969 | 0.115 | 15 | BGM, HAT | 0.0076 | 120.926 | 8.893 |
| NTP-5325QRI-SOL-S36-NIAR-WC-A-C2-1-RTD-5*** | A | C2 | 1 | 2 | 123.497 | | 0.115 | 15 | HAT, BGM | 0.0076 | 122.553 | |

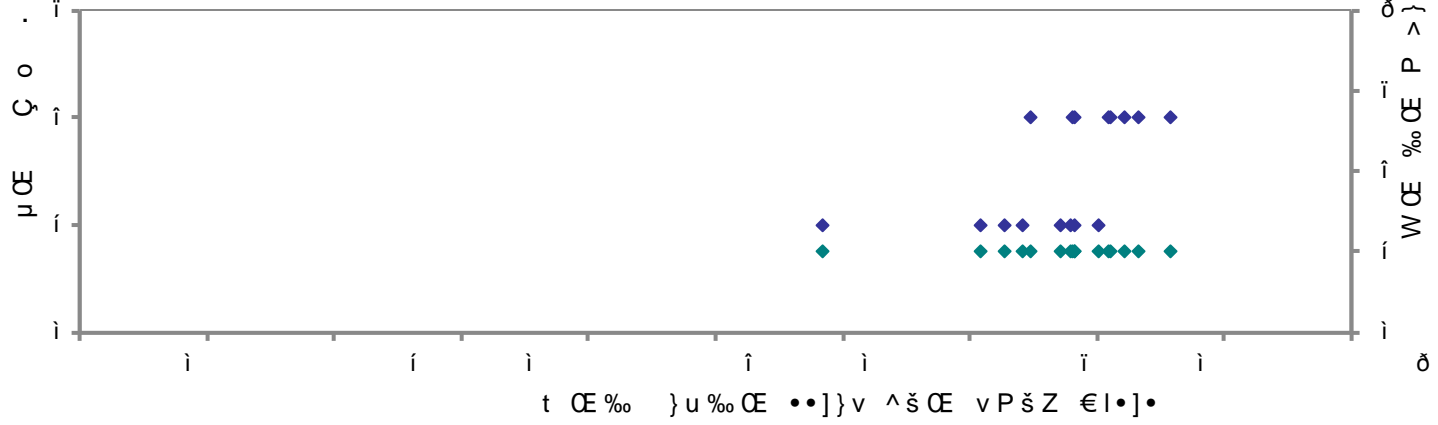
*Modulus are averaged values of 2 strain gages.
**Strength not reported due to unacceptable failure mode.
***Specimen was not gaged, only strength is tested.

| | | | | |
|--------------------|------------|----------------------------|------------|------------|
| 5jYFU[Y %&'%'&% | -'\$)(| 5jYFU[Y b c f a '\$\$\$+* | %&&'%' | ,'-,% |
| GhUbXUfX'8Yj' | \$%'+' | GhUbXUfX'8Yj' b c f a | '' ,) | \$%) , |
| 7cYZZ'cZ'JUf'0 i Q | '%*, %-\$- | 7cYZZ'cZ'JUf'0 i Q b c f a | '%) * | %'+*% |
| A]b' | %(') ++ | A]b' | \$\$\$+* | %''+\$% |
| AUI' | %&''+,* | AUI' | \$\$\$\$++ | %'&' , -\$ |
| Bi a VYf'cZ'GdYW' | , | Bi a VYf'cZ'GdYW' | - | , |

8YWY a VYf'9

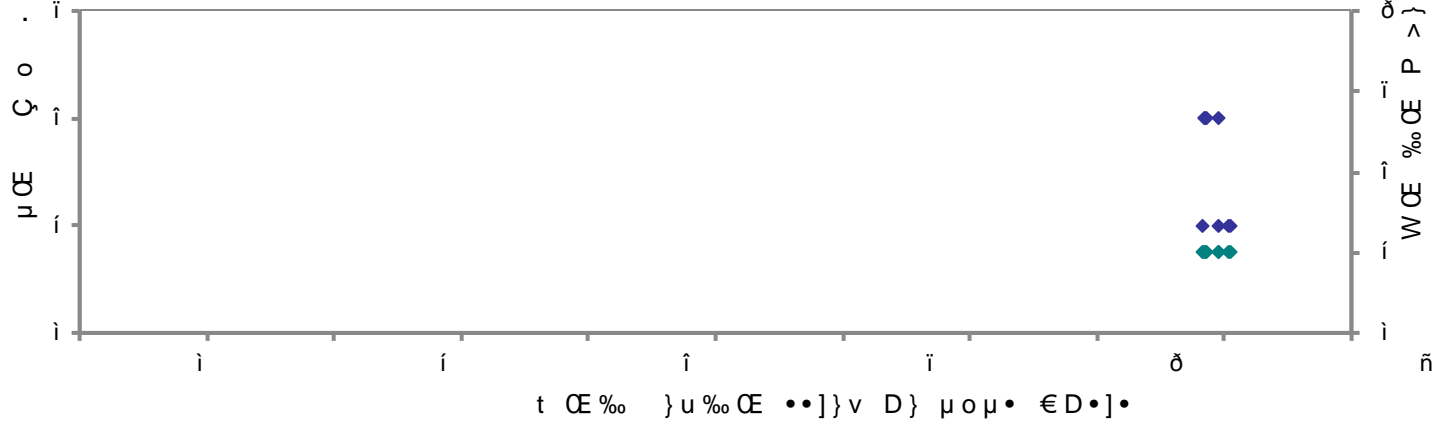
**KUfd'7c a dfYgg]cb'DfcdYfh]Ygfl K 7L!!9H K&
 Bcf aU`nYX'GhfYb[h\
 Solvay 5320-1 T650 3k-PW fabric with 36% RC**

◆ μ_{CE} ζ o .
 ◆ W_{CE} $\%_{CE}$ P > } \$.



**KUfd'7c a dfYgg]cb'DfcdYfh]Ygfl K 7L!!9H K&
 Bcf aU`nYX'AcXi`ig
 Solvay 5320-1 T650 3k-PW fabric with 36% RC**

◆ μ_{CE} ζ o .
 ◆ W_{CE} $\%_{CE}$ P > } \$.



8YWy a VYf %-ž&\$%-75 A!FD!&\$%-!\$()'FYj'B#7

("(' :]``7c a dfYgg]cb`DfcdYfh]Yg`fl : 7Ł`

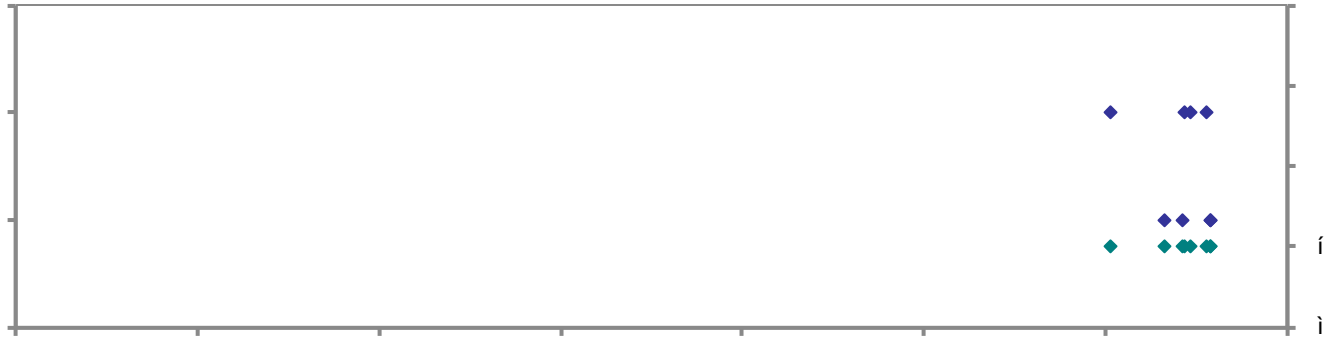
b c f a U ' n] b ['
h d m 0] b 0
0.0077

GdYW]a Yb`B i a VYf

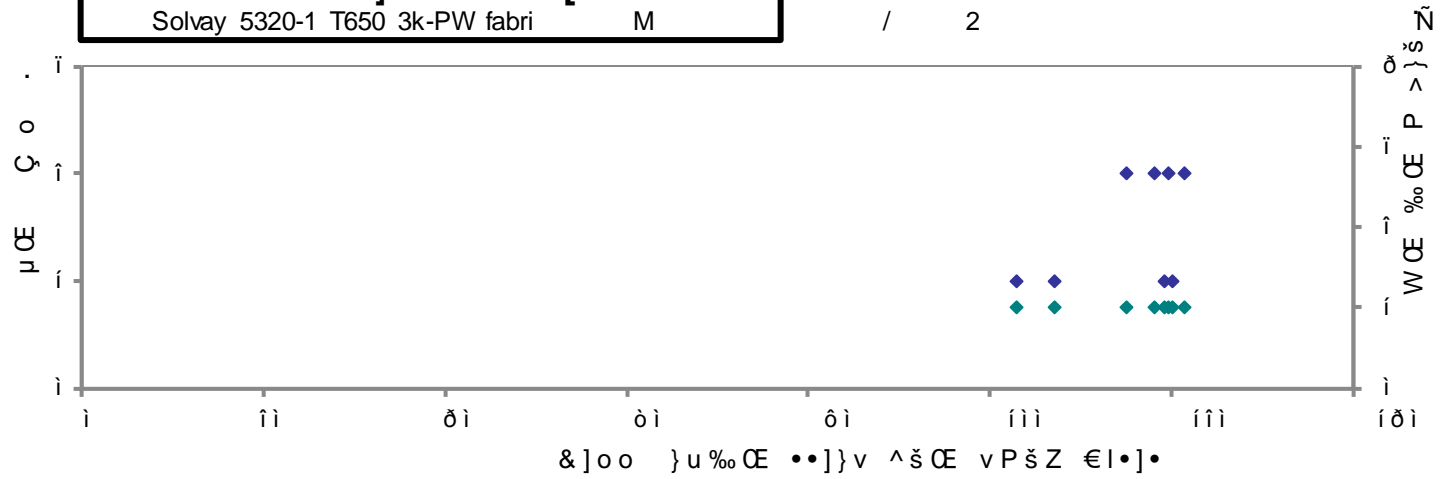
B-5F` B-5F` DfYdfY['@ch`
6UhW\` 7 i fY`7mW`Y`

8YWy a VYf %-ž&\$%-

.....75 A!FD!&\$%-!\$()'FYj`B#7



:]``7 c a dfYgg]cb`DfcdYfh]Ygñ: 7ł!!FH 8
Bcf a U`nYX`GhfYb [h
 Solvay 5320-1 T650 3k-PW fabri M / 2



8YWy a VYf %-ž&\$%-

.....75 A!FD!&\$%-!\$()'FYj`B#7



8YWY a VYf %-ž'&\$%- '75 A!FD!&\$%-!\$()'FYj`B#7

(") ` =b!D`UbY`G\YUf`DfcdYfh]Yg`fl=DGL`

GdYW]aYb`B i a VYf

B=5F`
6UhW\`

B=5F`
7 ifY`7mW`Y

DfYdfY[`@ch` 7 ifY`7mW`Y

\$& i`CZgYh`
GhfYb[h\
0_g]R

GhfYb[h\
) i`GifU]b
0_g]R

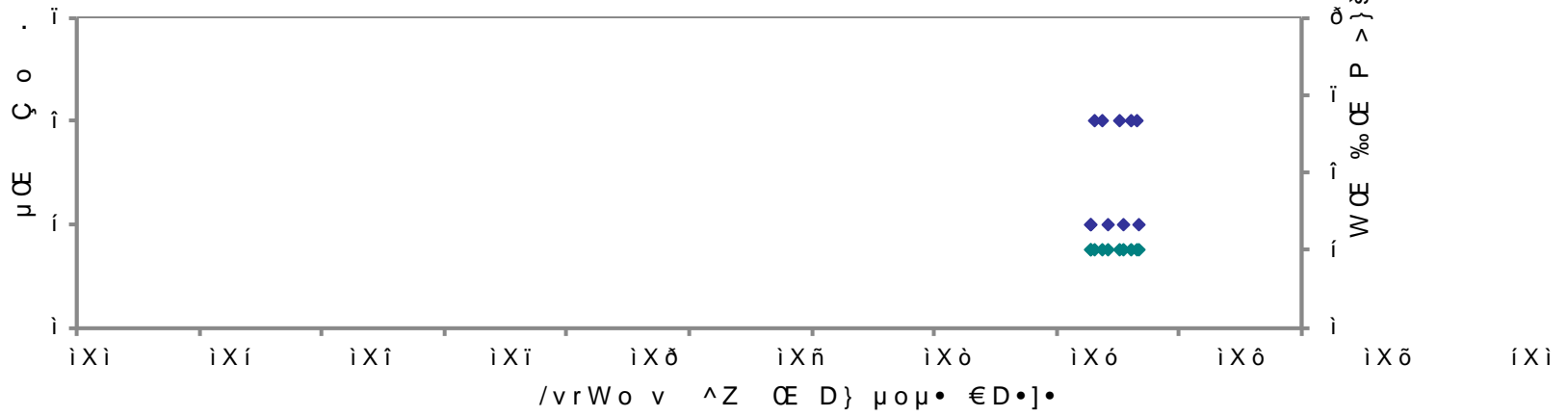
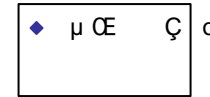
AcXi`i g`
0Ag]R

5 j[`
GdYW]aYb`
H\]W_bYgg`
0]bQ

`D]Yg]b`
@Ua]bUhY

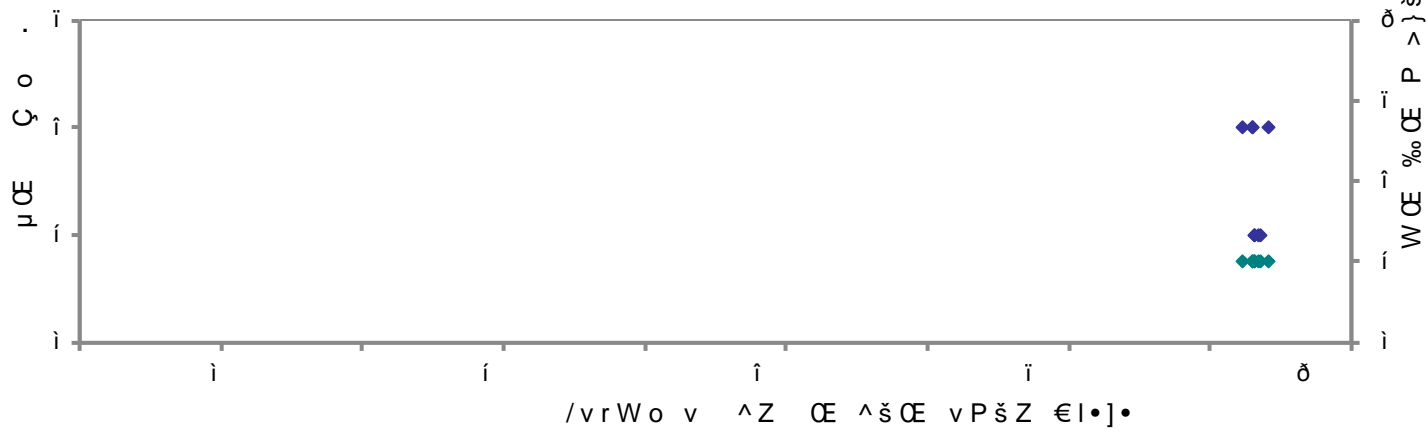
5 j[`h`d`m`0]bQ

=b!D`UbY'G\YUf'DfcdYfhjYgfl=DGL!!7H8
AYUg ifYX'AcXi`ig
Solvay 5320-1 T650 3k-PW fabric with 36% RC



=b!D`UbY`G\YUf`DfcdYfh]Ygřl=DGL!!FH 8
A YUg i fYX`\$"& i `CZgYh`GhfYb[h
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

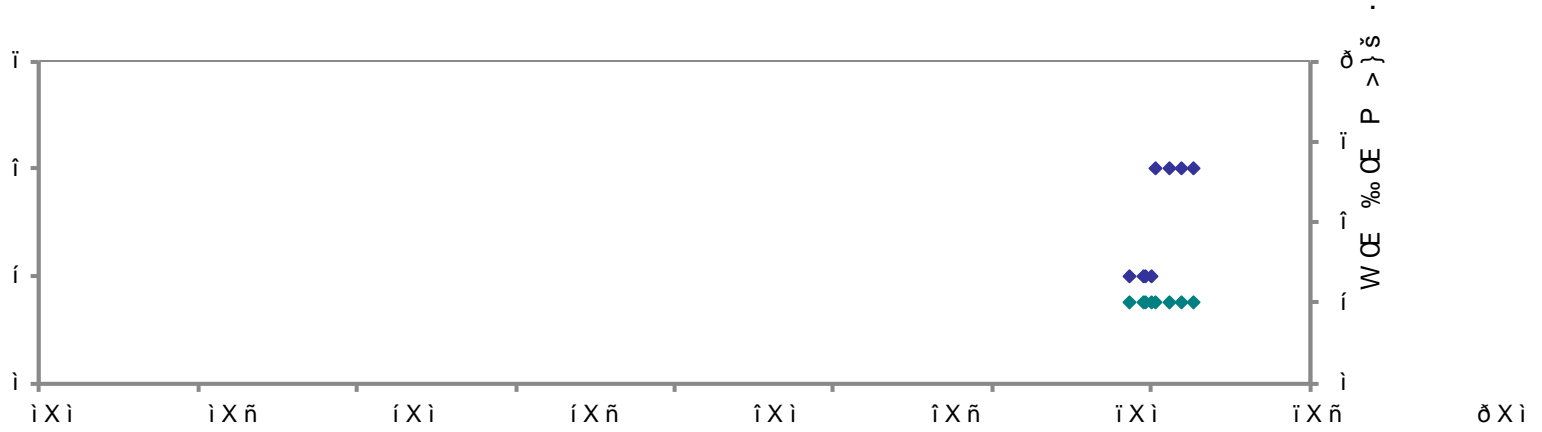
◆ μ OE Ç o .
 ◆ W OE %o OE P > } š .



ñ



8YWy a VYf %-ž'&\$%-'



8YWY a VYf %-ž'&\$%- '75 A!FD!&\$%-!\$()' FY j' B#7

("*' @U a]bU'G \cfh!6YU a 'GhfYb [h \ 'DfcdYfh]Yg'fIG6GŁ'

G \cfh!6YU a 'GhfYb [h \ 'DfcdYfh]Yg'fIG6GŁ!!7H8
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

| GdYW]a Yb'Bi a VYf | B-5F' 6UhW\ ' ı | B-5F' 7 i fY' 7mW'Y | DfYdfY['@ch' ı | 7 i fY' 7mW'Y ı | GhfYb [h \ 0_g]0 | 5 j ["" GdYW] a Yb' H \]W_bYgg' 0]b0 | 'D']Yg']b' @U a]bUhY | 5 j [""hdfm'0]b0 | :U] i fY' AcXY |
|---|-----------------|---------------------|-----------------|-----------------|------------------|---------------------------------------|-----------------------|------------------|-----------------------------|
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-CTD-1 | A | C1 | 1 | 1 | 14.385 | 0.244 | 32 | 0.0076 | INTERLAMINAR SHEAR, TENSION |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-CTD-2 | A | C1 | 1 | 1 | 15.070 | 0.243 | 32 | 0.0076 | INTERLAMINAR SHEAR, TENSION |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-CTD-3 | A | C1 | 1 | 1 | 13.810 | 0.243 | 32 | 0.0076 | INTERLAMINAR SHEAR, TENSION |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-CTD-4 | A | C1 | 1 | 1 | 14.816 | 0.243 | 32 | 0.0076 | INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-CTD-1 | A | C2 | 1 | 2 | 13.845 | 0.246 | 32 | 0.0077 | INTERLAMINAR SHEAR, TENSION |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-CTD-2 | A | C2 | 1 | 2 | 14.250 | 0.245 | 32 | 0.0077 | INTERLAMINAR SHEAR, TENSION |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-CTD-3 | A | C2 | 1 | 2 | 14.227 | 0.245 | 32 | 0.0077 | INTERLAMINAR SHEAR, TENSION |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-CTD-4 | A | C2 | 1 | 2 | 14.444 | 0.246 | 32 | 0.0077 | INTERLAMINAR SHEAR, TENSION |

5 jYfU[Y %(')* '\$\$\$+*
 GhUbXufX' 8Yj' \$(' ('
 7cYZZ' cZ' JUF''0 i Q '\$&&
 A]b' %'',%\$ '\$\$\$+*
 AUl' %)'\$+\$ '\$\$\$++
 Bi a VYf cZ' GdYW" , ,

G \cfh!6YU a 'GhfYb[h\`DfcdYfh]Yg'f!G6GL!!FH8
 Solvay 5320-1 T650 3k-PW fabric with 36% RC

| GdYW]a Yb'Bi a VYf | B-5F' 6UhW\` | B-5F' 7 ifY'7mW'Y | DfYdfY['@ch | 7 ifY'7mW'Y | GhfYb[h\ 0_g]Q | 5 j[" GdYW]a Yb' H\]W_bYgg' 0]bQ | 'D]Yg]b' @Ua]bUhY | 5 j["h_d'm'0]bQ | :U] ifY'AcXY |
|---|--------------|-------------------|-------------|-------------|----------------|----------------------------------|-------------------|-----------------|-----------------------------|
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-RTD-1 | A | C1 | 1 | 1 | 12.760 | 0.243 | 32 | 0.0076 | INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-RTD-2 | A | C1 | 1 | 1 | 12.932 | 0.243 | 32 | 0.0076 | INTERLAMINAR SHEAR, TENSION |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-RTD-3 | A | C1 | 1 | 1 | 12.948 | 0.244 | 32 | 0.0076 | INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-RTD-4 | A | C1 | 1 | 1 | 12.945 | 0.243 | 32 | 0.0076 | INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-RTD-1 | A | C2 | 1 | 2 | 13.180 | 0.244 | 32 | 0.0076 | INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-RTD-2 | A | C2 | 1 | 2 | 12.887 | 0.244 | 32 | 0.0076 | INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-RTD-3 | A | C2 | 1 | 2 | 12.779 | 0.244 | 32 | 0.0076 | INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-RTD-4 | A | C2 | 1 | 2 | 13.433 | 0.244 | 32 | 0.0076 | INTERLAMINAR SHEAR |

5 jYfU[Y %&-', '
 GhUbXUfX'8Yj' \$'&&' \$\$\$\$+*
 7cYZZ'cZ'JUf''0 i Q %'+%)
 A]b' %&+*\$ \$\$\$\$+*
 AUl' %''(' ' \$\$\$\$+*
 Bi a VYf cZ'GdYW" ,

| GdYW]a Yb' B i a VYf | B=5F' 6UhW\` | B=5F' 7 i fY' 7mW'Y | DfYdfY[@ch' 7 i fY' 7mW'Y | GhfYb[h\ 0_g]Q | 5 j[" GdYW]a Yb' H\]W_bYgg' 0]bQ | 'D]Yg]b' @Ua]bUhY | 5 j["h_drm'0]bQ | :U] i fY' AcXY |
|--|--------------|---------------------|---------------------------|----------------|----------------------------------|-------------------|-----------------|---------------------------|
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-ETW2-1 | A | C1 | 1 | 1 | 6.739 | 0.245 | 32 | 0.0076 INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-ETW2-2 | A | C1 | 1 | 1 | 6.762 | 0.244 | 32 | 0.0076 INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-ETW2-3 | A | C1 | 1 | 1 | 6.859 | 0.244 | 32 | 0.0076 INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C1-1-ETW2-4 | A | C1 | 1 | 1 | 6.866 | 0.244 | 32 | 0.0076 INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-ETW2-1 | A | C2 | 1 | 2 | 7.391 | 0.245 | 32 | 0.0077 INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-ETW2-2 | A | C2 | 1 | 2 | 7.087 | 0.245 | 32 | 0.0076 INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-ETW2-3 | A | C2 | 1 | 2 | 6.929 | 0.244 | 32 | 0.0076 INTERLAMINAR SHEAR |
| NTP-5325QRI-SOL-S36-NIAR-SBS-A-C2-1-ETW2-4 | A | C2 | 1 | 2 | 6.923 | 0.244 | 32 | 0.0076 INTERLAMINAR SHEAR |

5 jYfU[Y **-()
 GhUbXufX' 8Yj* \$%&\$
 7cYZZ" cZ' JUF"0 i Q '\$&*

 A]b* **+ ' -
 AUl' +'' -%
 B i a VYf cZ' GdYW' , H + -' 0

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$()`FYj`B#7

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$()'FYj`B#7

| | | | |
|-----------------------|--|--|--|
| bcfaU]n]b[| | | |
| h _d m'0]b0 | | | |
| 0.0077 | | | |

GdYW]a Yb`Bi a VYf

| | | | |
|--------|------------|------------------|----|
| B-5F' | B-5F' | DfYdfY['@ch - B | h' |
| 6UHW\` | 7 ifY'7mWY | | |

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$()'FYj`B#7



8YWy a VYf %-ž'&\$%-'

8YWy a VYf %-ž'&\$%-'

.....75A!FD!&\$%-!\$()'FYj`B#7

bcaU]nb[
hdm'0]b0
0.0077

GdYW]aYb`Bi a VYf

B-5F'
6UhW\`

B-5F'
7ifY'7mWY

DfYdfY['@ch' 7ifY'7mWY'

GhfYb[h\
0_g]R

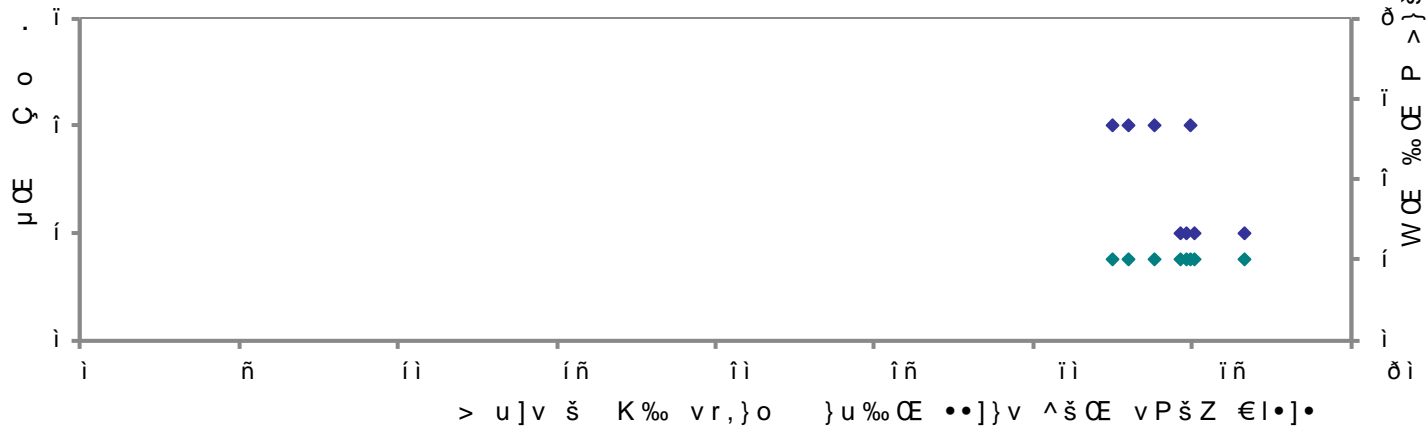
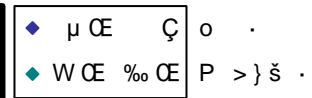
5j["
GdYW]aYb`
H\]W_bYgg'
0]b0

`D]Yg]b`
@Ua]bUhY

:U]ifY`AcXY

5j["hdm'0]b0

@U a]bUhY`CdYb!<c`Y`7c a dfYgg]cb`DfcdYfh]Yg`flC<7%k!!9HK&
Bcf aU`nYX`GhfYb [h
 Solvay 5320-1 T650 3k-PW fabric with 36% RC



8YWy a VYf %-ž'&\$%-

.....75 A!FD!&\$%-!\$()'FYj'B#7

("-' Í&#)\$&#) Î'7c a dfYgg]cb'GhfYb [h\ '5ZhYf'= a dUWh'% 'DfcdYfh]Yg'fl7 5=%k'

| |
|---|
| <p>@Ua]bUhY'7c a dfYgg]cb'5ZhYf'= a dUWh'% 'DfcdYfh]Yg'fl7 5=%k!!FH8</p> <p>GhfYb[h\</p> <p>Solvay 5320-1 T650 3k-PW fabric with 36% RC</p> |
|---|

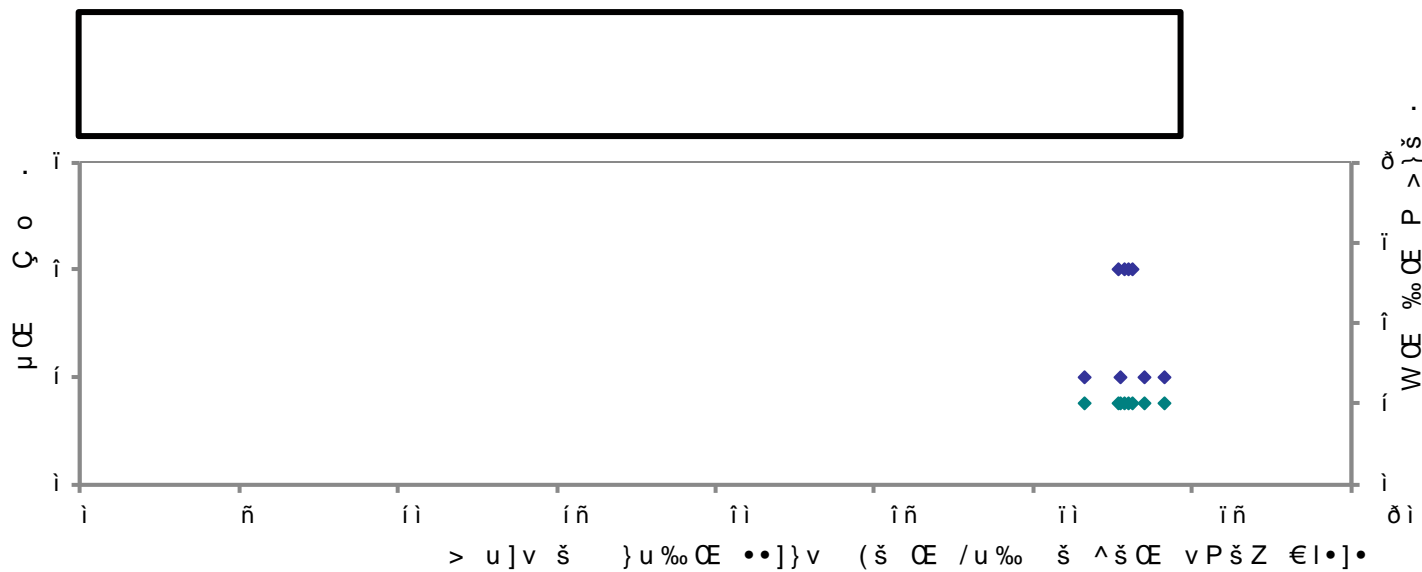
| |
|---------------|
| bcf a U]n]b [|
| h_d m'0]b0 |
| 0.0077 |

| GdYW]a Yb'Bi a VYf | B=5F' 6UhW\` | B=5F' 7ifY'7mW'Y | DfYdfY['@ch | 7ifY'7mW'Y | GhfYb[h\ 0_g]0 | AYUg ifYX' = a dUWh' 9bYf [m 0]b'VZ0 | 5j ["" GdYW]a Yb' H\W_bYgg' 0]b0 | 'D]Yg]b' @Ua]bUhY | :U] ifY'AcXY |
|--|--------------|------------------|-------------|------------|----------------|--------------------------------------|----------------------------------|-------------------|--------------|
| NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C1-1-RTD-1 | A | C1 | 1 | 1 | 34.241 | 273.46 | 0.184 | 24 | LDM |
| NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C1-1-RTD-2 | A | C1 | 1 | 1 | 32.716 | 280.41 | 0.185 | 24 | LDM |
| NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C1-1-RTD-3 | A | C1 | 1 | 1 | 31.537 | 277.66 | 0.185 | 24 | LDM |
| NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C1-1-RTD-4 | A | C1 | 1 | 1 | 33.465 | 280.03 | 0.185 | 24 | LDM |
| NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C2-1-RTD-1 | A | C2 | 1 | 2 | 32.504 | 280.79 | 0.186 | 24 | LDM |
| NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C2-1-RTD-2 | A | C2 | 1 | 2 | 32.908 | 280.37 | 0.186 | 24 | LDM |
| NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C2-1-RTD-3 | A | C2 | 1 | 2 | 32.905 | 280.17 | 0.185 | 24 | LDM |
| NTP-5325QRI-SOL-S36-NIAR-CAI1-A-C2-1-RTD-4 | A | C2 | 1 | 2 | 32.713 | 280.07 | 0.186 | 24 | LDM |

| 5j [""h_d m'0]b0 | GhfYb[h\bcfa 0_g]0 |
|------------------|--------------------|
| 0.0077 | 34.104 |
| 0.0077 | 32.716 |
| 0.0077 | 31.583 |
| 0.0077 | 33.478 |
| 0.0077 | 32.700 |
| 0.0077 | 33.115 |
| 0.0077 | 33.008 |
| 0.0077 | 32.841 |

5jYfU[Y '&',+'
 GhUbXUfX'8Yj" '\$'++(
 7cYZZ'cZ'JUf''0 i 0 &''))
 A]b" '%)'+'
 AU1" '(&(%
 Bi a VYf'cZ'GdYW" ,

5jYfU[Ybcfa '\$\$\$++ '&'-'
 GhUbXUfX'8Yj'bcfa '\$'+&%
 7cYZZ'cZ'JUf''0 i 0bcfa &'%, ,
 A]b" '\$\$\$++ '%)', '
 AU1" '\$\$\$++ '(%\$(\$
 Bi a VYf'cZ'GdYW" ,



)" 5XX]h]cbU`7 c a dfYgg]cb' 5ZhYf' = a dUWh' 8UhU'

Impactor Diameter: 0.625"

Representative of Damage Area:



Damage Area and Dent Depth Summary:

| GdYW] a Yb':8' | 8U a U[Y' 5fYU f]bW\&L' | 8Ybh' 8Ydh\ f]bW\&L' |
|--|----------------------------|-------------------------|
| NTP-5325QR1-SOL-S36-NIAR-CAI1-A-C1-1-RTD-1 | 0.0335 | 1.179 |
| NTP-5325QR1-SOL-S36-NIAR-CAI1-A-C1-1-RTD-2 | 0.0375 | 1.403 |

8YWY a VYf %-ž&\$%- 75A!FD!&\$%-!\$()'FYj'B#7

*'' K Ufd'7c a dfYgg]cb'Ë'FH8'

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| | | | | |
| | | | | |

8YWy a VYf %-ž&\$%-75A!FD!&\$%-!\$()'FYj'B#7

+'' Ac]gh i fY'7cbX]h]cb]b['7\Ufhg'

+ "%' =b!D`UbY`G\YUf`Ë`H\]bbYgh`DUbY`

, " 8A5'FYgi'hg'

| 8A5'FYgi'hg'Gi a aUfm'! : 55'FYdUJf' E i U'Z]WUh]cb BHD!) '&)EF=!GC@!G' *!B=5F' 8A5'8fm'fl9e i]jU'YbWmł | | | | |
|---|-----------------------|---------|----------------------|---------|
| GUad'Y' | CbgYh'GhcfU[Y'AcXi'ig | | DYU_cZHUb[Ybhi'8Y'hU | |
| | H1'0š7Q | H1'0š:Q | H1'0š7Q | H1'0š:Q |
| CAI1-A-C1-1-DMA-D | 200.52 | 392.94 | 214.27 | 417.69 |
| CAI1-A-C2-1-DMA-D | 201.11 | 394.00 | 214.75 | 418.55 |
| FC-A-C1-1R-DMA-D | 202.72 | 396.90 | 220.27 | 428.49 |
| FC-A-C2-1R-DMA-D | 203.52 | 398.34 | 221.87 | 431.37 |
| FT-A-C1-1R-DMA-D | 203.11 | 397.60 | 220.73 | 429.31 |
| FT-A-C2-1R-DMA-D | 203.50 | 398.30 | 220.38 | 428.68 |
| IPS-A-C1-1-DMA-D | 195.17 | 383.31 | 211.41 | 412.54 |
| IPS-A-C2-1-DMA-D | 195.76 | 384.37 | 212.33 | 414.19 |
| OHC1-A-C1-1-DMA-D | 201.98 | 395.56 | 218.12 | 424.62 |
| OHC1-A-C2-1-DMA-D | 199.54 | 391.17 | 214.49 | 418.08 |
| OHT1-A-C1-1-DMA-D | 198.05 | 388.49 | 215.18 | 419.32 |
| OHT1-A-C2-1-DMA-D | 198.29 | 388.92 | 215.73 | 420.31 |
| SBS-A-C1-1-DMA-D | 204.73 | 400.51 | 215.03 | 419.05 |
| SBS-A-C2-1-DMA-D | 203.12 | 397.62 | 215.32 | 419.58 |
| WC-A-C1-1-DMA-D | 198.89 | 390.00 | 214.72 | 418.50 |
| WC-A-C2-1-DMA-D | 201.47 | 394.65 | 218.48 | 425.26 |
| WT-A-C1-1-DMA-D | 198.79 | 389.82 | 214.59 | 418.26 |
| WT-A-C2-1-DMA-D | 199.99 | 391.98 | 216.46 | 421.63 |
| Average | 200.57 | 393.03 | 216.34 | 421.41 |
| Standard Deviation | 2.73 | 4.91 | 2.97 | 5.35 |

| 8A5'FYgi'hg'Gi a aUfm'! : 55'FYdUJf' E i U'Z]WUh]cb BHD!) '&)EF=!GC@!G' *!B=5F' 8A5'KYh'fl9e i]jU'YbWmł | | | | |
|---|-----------------------|---------|----------------------|---------|
| GUad'Y' | CbgYh'GhcfU[Y'AcXi'ig | | DYU_cZHUb[Ybhi'8Y'hU | |
| | H1'0š7Q | H1'0š:Q | H1'0š7Q | H1'0š:Q |
| CAI1-A-C1-1-DMA-W | 159.01 | 318.22 | 173.93 | 345.07 |
| CAI1-A-C2-1-DMA-W | 158.37 | 317.07 | 173.89 | 345.00 |
| FC-A-C1-1R-DMA-W | 156.99 | 314.58 | 171.16 | 340.09 |
| FC-A-C2-1R-DMA-W | 156.41 | 313.54 | 170.95 | 339.71 |
| FT-A-C1-1R-DMA-W | 157.59 | 315.66 | 171.43 | 340.57 |
| FT-A-C2-1R-DMA-W | 158.82 | 317.88 | 171.78 | 341.20 |
| IPS-A-C1-1-DMA-W | 145.98 | 294.76 | 167.39 | 333.30 |
| IPS-A-C2-1-DMA-W | 145.64 | 294.15 | 167.56 | 333.61 |
| OHC1-A-C1-1-DMA-W | 157.96 | 316.33 | 173.93 | 345.07 |
| OHC1-A-C2-1-DMA-W | 156.79 | 314.22 | 172.69 | 342.84 |
| OHT1-A-C1-1-DMA-W | 156.63 | 313.93 | 171.93 | 341.47 |
| OHT1-A-C2-1-DMA-W | 157.01 | 314.62 | 173.29 | 343.92 |
| SBS-A-C1-1-DMA-W | 161.88 | 323.38 | 174.23 | 345.61 |
| SBS-A-C2-1-DMA-W | 161.14 | 322.05 | 174.30 | 345.74 |
| WC-A-C1-1-DMA-W | 158.02 | 316.44 | 171.82 | 341.28 |
| WC-A-C2-1-DMA-W | 158.83 | 317.89 | 172.98 | 343.36 |
| WT-A-C1-1-DMA-W | 157.61 | 315.70 | 170.59 | 339.06 |
| WT-A-C2-1-DMA-W | 157.38 | 315.28 | 171.15 | 340.07 |
| Average | 156.78 | 314.21 | 171.94 | 341.50 |
| Standard Deviation | 4.25 | 7.64 | 2.03 | 3.66 |

8YWy a VYf %-ž&\$%-`

8YWy a VYf %-ž&\$%-

.....75A!FD!&\$%-!\$()`FYj`B#7