

See e_j a , f , d c ac , cc , , a d
a a a

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“... (2001, 2002) ...”

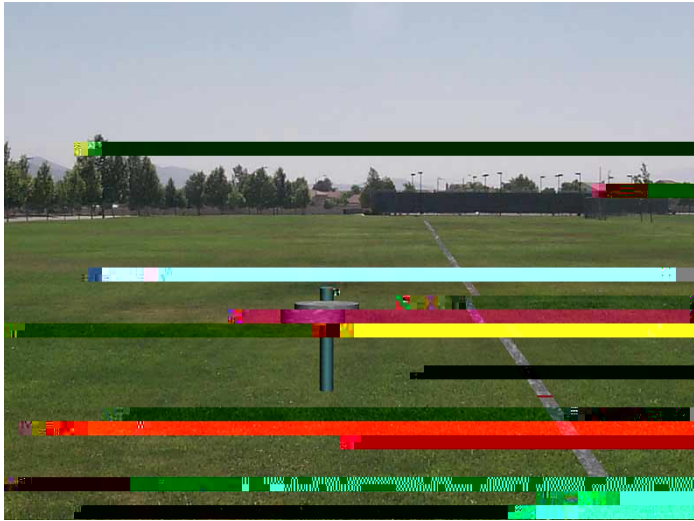


Fig. 1. [Illegible text due to heavy redaction]

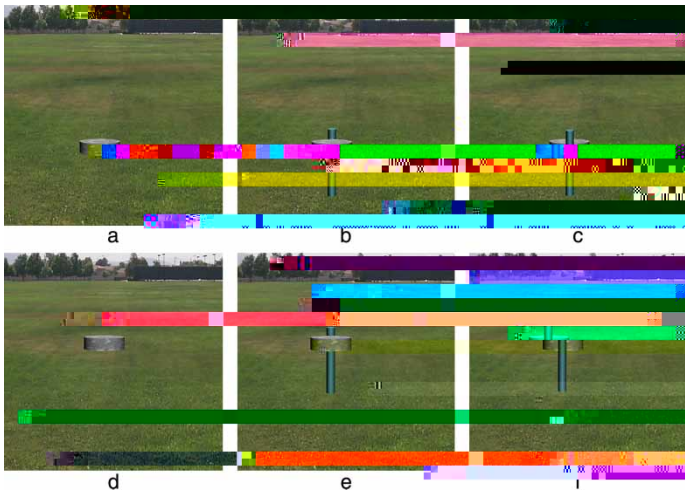


Fig. 2. [Illegible text due to heavy redaction]

... (...) ... 1% ... 5 ... 20% ...

Design.

... (...) ... 10 ... 20 ...

Procedure.

... (... & ... , 2001, 2002 ... , 2005), ... (...) ...

s s i sD s\$

... 3 ... j ... t ... F(2, 22)=6.3, MSE=7.74, p<.01, ... F(1, 11)=462.7, MSE=2.5, p<.01, ... F(2, 22)=7.25, MSE=1.05, p<.01. ... p<.05, ... 3, t j ... (...) ... & ... , 2002).

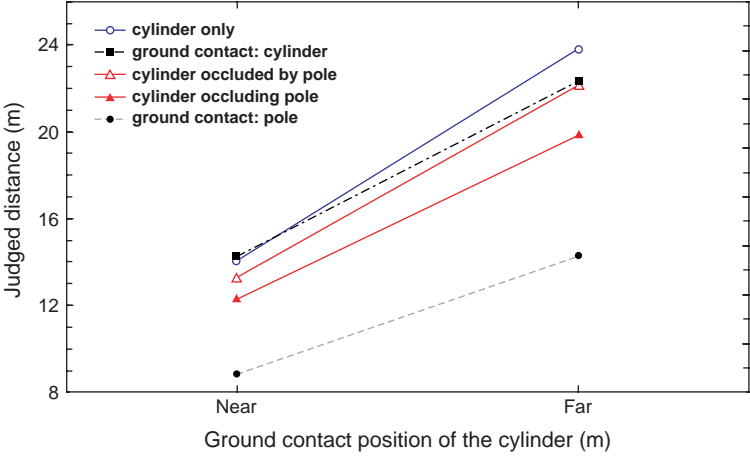


Figure 3. Effect of ground contact position on judged distance for different occlusion conditions.

The results show that judged distance increases with ground contact position for all conditions. The increase is most pronounced for the 'cylinder only' condition, where the distance is judged to be 23.5m at the Far position compared to 14.5m at the Near position. The 'ground contact: pole' condition shows the smallest increase, from 9.0m at the Near position to 14.5m at the Far position.

The 'ground contact: cylinder' condition shows a similar increase in judged distance as the 'cylinder only' condition, from 14.5m at the Near position to 22.0m at the Far position. The 'cylinder occluded by pole' and 'cylinder occluding pole' conditions also show an increase in judged distance, with the latter showing a slightly larger increase from 12.5m at the Near position to 20.0m at the Far position.

The results also show that the presence of a pole affects the judged distance. The 'cylinder occluded by pole' and 'cylinder occluding pole' conditions show lower judged distances compared to the 'cylinder only' condition. This suggests that the presence of a pole reduces the perceived distance between the cylinder and the observer.

The 'ground contact: pole' condition shows the lowest judged distance at both the Near and Far positions. This is likely due to the fact that the pole is the only point of contact, which makes the distance appear shorter than when the cylinder itself is in contact with the ground.

Overall, the results indicate that judged distance is highly dependent on the ground contact position and the presence of occluding objects. The 'cylinder only' condition consistently yields the highest judged distances, while the 'ground contact: pole' condition yields the lowest.

The data points for the 'ground contact: cylinder' condition are 14.5m at the Near position and 22.0m at the Far position. The data points for the 'cylinder occluded by pole' condition are 13.5m at the Near position and 21.5m at the Far position. The data points for the 'cylinder occluding pole' condition are 12.5m at the Near position and 20.0m at the Far position. The data points for the 'ground contact: pole' condition are 9.0m at the Near position and 14.5m at the Far position.

E X E I M E N 2: M O I O N A A L L A X A N D O C C L I O N

1. $\frac{1}{2} \frac{d}{dt} (m v^2) = \mathbf{F} \cdot \mathbf{v}$ (work-energy theorem)

2. $\mathbf{F} = -\nabla U$ (conservative force)

3. $\mathbf{L} = \mathbf{r} \times \mathbf{p}$ (angular momentum)

4. $\frac{d\mathbf{L}}{dt} = \mathbf{r} \times \mathbf{F}$ (torque)

5. $\mathbf{L} = I \boldsymbol{\omega}$ (rotational inertia)

6. $\tau = I \alpha$ (rotational Newton's second law)

7. $U = \frac{1}{2} I \omega^2$ (rotational kinetic energy)

8. $\mathbf{L} = \int \mathbf{r} \times \mathbf{p} \, dm$ (continuous mass distribution)

9. $\mathbf{L} = \int \mathbf{r} \times \mathbf{p} \, dm$ (continuous mass distribution)

10. $\mathbf{L} = \int \mathbf{r} \times \mathbf{p} \, dm$ (continuous mass distribution)

M

Observers. 11. $\mathbf{L} = \int \mathbf{r} \times \mathbf{p} \, dm$ (continuous mass distribution)

12. $\mathbf{L} = \int \mathbf{r} \times \mathbf{p} \, dm$ (continuous mass distribution)

13. $\mathbf{L} = \int \mathbf{r} \times \mathbf{p} \, dm$ (continuous mass distribution)

14. $\mathbf{L} = \int \mathbf{r} \times \mathbf{p} \, dm$ (continuous mass distribution)

15. $\mathbf{L} = \int \mathbf{r} \times \mathbf{p} \, dm$ (continuous mass distribution)

1. $\frac{d}{dt} \left(\frac{1}{t} \right) = -\frac{1}{t^2}$

Procedure. ... t t t ... t 1-3,
t t t ... t j t t t t t
t ...

s s | sD s\$
T 3 (i) 3487 1
p < .05, F(4, 27) = 3. MS = 6.5
F(4, 27) = 3. SE ... p < .05

GENERAL DISCUSSION

... , ... t ... t t t t t j ... t ... j t 3-
... t ... t ... t ... t ... t ...
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t , t t t t t j t .
t t t t t t t t
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t (C. J. C. J., 2005). . . . t . . . t . . . t . . . t . . .

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Manuscript received July 2005
Manuscript accepted November 2005
First published online June 2006